March 6, 2020
St. Clair County Industrial Park
Moody, AL
Traffic Impact Analysis

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## SAIN PROJECT \#:

190119

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B. Raw Traffic Count Data
C. Description of Levels of Service
D. Background Conditions Capacity Analysis
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## Other Information

Sources of information other than Sain Associates used in preparation of this traffic impact analysis include:

- Alabama Department of Transportation (ALDOT)
- Transportation Research Board (TRB)
- Traffic Data, LLC
- Google Earth
- Capstone Real Estate Investments


## Executive Summary

Sain Associates examined the traffic impacts associated with a proposed industrial park in Moody, Alabama. The purpose of this study is to analyze the traffic conditions in the vicinity of the proposed development, determine any impact that the proposed development may have on the existing traffic network, and recommend any improvements that may be necessary to mitigate any impacts.

The proposed development is located on the northwestern side of Kelly Creek Road, approximately 1.25 miles north of the I-20/Kelly Creek Road interchange. The site is currently a wooded area. According to the site plan, the proposed facility will be located on a 172 acre site and will have one access on Kelly Creek Road.

Based on our observations and analysis documented in this report, Sain Associates makes the following recommendations/conclusions:

- The study intersections are projected to continue to operate with acceptable LOS during the future peak periods, except for the Park Avenue approaches to Kelly Creek Road.
- Construct a right turn lane on the southbound Kelly Creek Road approach to the Proposed Driveway. The turn lane should be at least 275 feet in length, with 175 feet of storage length and 100 feet of taper length.
- Construct a left turn lane on the northbound Kelly Creek Road approach to the Proposed Driveway. The turn lane should be at least 275 feet in length, with 175 feet of storage length and 100 feet of taper length.


## Purpose

Sain Associates examined the traffic impacts associated with a proposed industrial park development in Moody, Alabama. The purpose of this study is to analyze the traffic conditions in the vicinity of the proposed development, determine any impact that the proposed development may have on the existing traffic network, and recommend any improvements that may be necessary to mitigate any impacts.

## Existing Conditions

## Site Description

The proposed development site is located on the northwestern side of Kelly Creek Road, approximately 1.25 miles north of the I-20/Kelly Creek Road interchange. The site is currently a wooded land use. According to the site plan, the proposed facility will be located on a 172 acre site and will have one full-directional access on Kelly Creek Road. We assumed approximately 142 acres were developable.

Figure 1 shows the site location as it relates to the surrounding roadway network. The full site plan is included in Appendix A.


Figure 1: Site Location

## Analysis Boundaries

Our analysis includes a review of traffic operations at the following locations:

- Kelly Creek Road at Proposed Driveway
- Kelly Creek Road at Park Avenue
- Kelly Creek Road at I-20 Westbound Ramp
- Kelly Creek Road at I-20 Eastbound Ramp


## Roadway Characteristics

Roadways within the study boundary exhibit the following characteristics:

- Kelly Creek Road is a two-lane, undivided, north-south roadway that is classified as a major collector. It has a posted speed limit ranging between 30-35 miles per hour within the study area, with the 35 miles per hour posted speed limit at the site location.
- Park Avenue is a two-lane, east-west roadway that is classified as a major collector. It has a posted speed limit of 45 miles per hour.
- $\underline{\underline{I}-20}$ is a six-lane, east-west roadway that is classified as an interstate. It has a posted speed limit of 70 miles per hour.


## Site Accessibility

Currently, there is one unpaved access connection to the proposed industrial park site on Kelly Creek Road. It is proposed that there will be one full access connection to the site under post-development conditions as well.

## Existing Traffic Volumes

Sain Associates, Inc. performed traffic data collection through sub-consultant Traffic Data, LLC. The turning movement count data was collected at the study intersections from 7:00-9:00 AM and from 4:00-6:00 PM on Wednesday, January 8, 2020. The AM and PM peak hours of traffic flow during these study periods were determined to be 7:00-8:00 AM and 4:30-5:30 PM.

Additionally, 24-hour bi-directional machine counts were collected on Kelly Creek Road, in front of the proposed access connection. These counts were also collected on Wednesday, January 8, 2019 and included vehicle, speed, and classification counts.

The existing 24 -hour volumes are summarized in Table 1, the existing peak hour traffic volumes are illustrated in Figure 2, and the raw traffic count reports are included as Appendix B.

Table 1: Existing 24-hour Volumes

| Location | Northbound | Southbound | Total |
| :---: | :---: | :---: | :---: |
| Kelly Creek Rd, between <br> Park Ave and Kerr Rd | 2,493 | 2,552 | 5,045 |



Figure 2: Existing Traffic Volumes

## Capacity Analysis and Levels of Service

Using the methods described in the Highway Capacity Manual, published by the Transportation Research Board, we analyzed the existing traffic conditions within the study area.

According to this method of analysis, traffic capacities are expressed as levels of service (LOS) ranging from "A" to "F." A detailed description of each LOS designation is included in Appendix C. Generally, LOS "C" is considered desirable, while LOS "D" is considered acceptable during peak hours of traffic flow.

There is a planned improvement project at the interchange of Kelly Creek Road and l-20 that will widen both exit ramps to two lanes. Because this interchange project is expected to be constructed prior to the Industrial Park becoming operational, the future geometry was considered the "background" condition for this analysis.

Full printouts of the background conditions capacity analysis are provided in Appendix D, with the results summarized in Table 2.

| Intersection | Approach |  | Level of Service |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak | PM Peak |
| Kelly Creek Rd @ Park Ave | EB | Park Ave | D | C |
|  | WB | Park Ave | F | C |
|  | NB | Kelly Creek Rd | A | A |
|  | SB | Kelly Creek Rd | A | A |
| Kelly Creek Rd @ I-20 WB Ramps | WB | I-20 WB Exit Ramp | C | C |
|  | NB | Kelly Creek Rd | A | A |
|  | SB | Kelly Creek Rd | A | A |
| Kelly Creek Rd @ I-20 EB Ramps | EB | I-20 EB Exit Ramp | B | C |
|  | NB | Kelly Creek Rd | C | C |
|  | SB | Kelly Creek Rd | C | C |
|  | Total Intersection LOS |  | C | C |

The study intersections are projected to operate with acceptable LOS for the background conditions, except for the westbound Park Avenue approach during the AM peak hour. It is not uncommon for a side-street stop controlled intersection to have an unacceptable LOS on the side-street approaches when volumes on a two-lane road are high.

## Future Traffic Operations Analysis

## Trip Generation

Sain Associates, Inc. estimated the number of vehicle trips to be generated by the proposed development using traffic counts collected at the existing Jefferson Metropolitan Industrial Park in McCalla, Alabama. It was assumed that there would be 10,000 gross square feet per developable acre. Traffic generated by a proposed development is often classified in two ways: new trips or pass-by trips. New trips are defined as vehicles whose primary destination is the proposed development; these trips are assumed to return to the same direction in which they arrived. Pass-by trips are defined as vehicles that stop into a development while headed to another destination. For the proposed industrial park facility there were assumed to be no pass-by trips during the peak study hours. A summary of the trip generation estimate is shown in Table 3.

Table 3: Trip Generation

| Peak Period | IN | OUT | TOTAL |
| :---: | :---: | :---: | :---: |
| AM | 127 | 72 | 199 |
| PM | 108 | 176 | 284 |

## Trip Distribution

The directional distribution of the new trips expected to be generated by the proposed development was estimated based on the population distribution within a 15 -mile radius of the proposed industrial park.

The directional distribution percentages of site-generated trips are illustrated in Figure 3.

## Trip Assignment

Using the aforementioned patterns of distribution, Sain Associates assigned the projected new trips to the site's proposed access system. The assigned volumes were then added to the background traffic volumes in order to produce future traffic volumes. The assigned traffic is illustrated in the following figures:

- Figure 4 - New Trips
- Figure 5 - Future Traffic Volumes


Figure 3: New Trip Distribution


Figure 4: New Trips


Figure 5: Fułure Traffic Volumes

## Capacity Analysis \& Levels of Service

Using the Highway Capacity Manual methods previously described for background capacity analysis, future traffic conditions within the study area were analyzed. Capacity analysis of future traffic conditions include our recommended geometric and traffic control improvements, which will be described in detail later in this report.

Full printouts of the future conditions capacity analysis are provided in Appendix E , with the LOS results summarized in Table 4.

| Intersection | Approach |  | Level of Service |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak | PM Peak |
| Kelly Creek Rd @ Proposed Driveway | EB | Prop. Driveway | C | B |
|  | NB | Kelly Creek Rd | A | A |
|  | SB | Kelly Creek Rd | A | A |
| Kelly Creek Rd @ Park Ave | EB | Park Ave | E | E |
|  | WB | Park Ave | F | D |
|  | NB | Kelly Creek Rd | A | A |
|  | SB | Kelly Creek Rd | A | A |
| Kelly Creek Rd @ I-20 WB Ramps | WB | I-20 WB Exit Ramp | C | C |
|  | NB | Kelly Creek Rd | A | A |
|  | SB | Kelly Creek Rd | A | A |
| Kelly Creek Rd @ I-20 EB Ramps | EB | I-20 EB Exit Ramp | B | D |
|  | NB | Kelly Creek Rd | C | C |
|  | SB | Kelly Creek Rd | D | C |
|  | Total Intersection LOS |  | C | C |

According to our capacity analysis, the study intersections are projected to continue to operate with acceptable LOS during the future AM peak period, except for the eastbound and westbound approaches at the intersection of Kelly Creek Road and Park Avenue. During the PM peak period, all of the study intersections are projected to continue to operate with acceptable LOS with the exception of the eastbound Park Avenue approach to the Kelly Creek Road intersection. As previously stated, it is not uncommon for stop-controlled side street approaches to have unacceptable LOS during peak periods of traffic. It should be noted that the westbound Park Avenue approach only had 17 vehicles during the AM peak hour.

## Turn Lane Warrants

Utilizing the information contained in NCHRP Report 457, turn lane warrant analyses were performed using the projected future volumes at the Proposed Driveway. Although the posted speed limit on this segment of Kelly Creek Road is 35 miles per hour, the collected speed data showed an $85^{\text {th }}$ percentile speed of 48 mph . For the purposes of this turn lane warrant analyses, a 45 mph speed was used. The inputs and results from those warrants are summarized in Table 5 and Table 6. Full printouts of the turn lane warrant analysis are provided in Appendix F.

|  | Peak Period | Major Road Volume (veh/h) | Turn | Turn Lane Warranted? |
| :---: | :---: | :---: | :---: | :---: |
| Approach |  |  | Volume (veh/h) |  |
| SB Kelly Creek Rd <br> @ Prop. Driveway | AM | 671 | 37 | YES |
|  | PM | 138 | 31 | NO |

Table 6: Left Turn Lane Warrant Evaluation

| Approach | Peak <br> Period | Major Road <br> Volume <br> (veh/h) | Turn <br> Volume <br> (veh/h) | Opposing <br> Volume <br> (veh/h) | Turn Lane <br> Warranted? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NB Kelly Creek Rd <br> @ Prop. Driveway | AM | 207 | 90 | 671 | YES |
|  | PM | 497 | 77 | 138 | YES |

Based on the projected future conditions, a right turn lane is warranted on the southbound approach, and a left turn lane is warranted on the northbound approach of Kelly Creek Road at the Proposed Driveway.

## Recommendations

Based on our observations and analysis documented in this report, Sain Associates makes the following recommendations/conclusions:

- The study intersections are projected to continue to operate with acceptable LOS during the future peak periods, except for the Park Avenue approaches to Kelly Creek Road.
- Construct a right turn lane on the southbound Kelly Creek Road approach to the Proposed Driveway. The turn lane should be at least 275 feet in length, with 175 feet of storage length and 100 feet of taper length.
- Construct a left turn lane on the northbound Kelly Creek Road approach to the Proposed Driveway. The turn lane should be at least 275 feet in length, with 175 feet of storage length and 100 feet of taper length.

APPENDIX A
Proposed Site Development Plan


## APPENDIX B <br> Raw Traffic Count Data

TRAFFIC DATA, LLC
1409 Turnham Lane
Moody, AL

Birmingham, AL 35216
205-824-0125

File Name : moody03
Site Code : 00000000
Start Date : 01/08/2020
Page No : 1

Groups Printed- Unshifted

|  | KELLY CREEK PKWY <br> Southbound |  | KELLY CREEK PKWY Northbound |  | 1-20 EB EXIT RAMP <br> Eastbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Thru | Right | Left | Thru | Right | Int. Total |
| 07:00 AM | 28 | 60 | 90 | 29 | 10 | 0 | 45 | 262 |
| 07:15 AM | 29 | 71 | 95 | 20 | 16 | 1 | 32 | 264 |
| 07:30 AM | 31 | 63 | 87 | 25 | 14 | 0 | 39 | 259 |
| 07:45 AM | 18 | 66 | 52 | 26 | 15 | 0 | 43 | 220 |
| Total | 106 | 260 | 324 | 100 | 55 | 1 | 159 | 1005 |
| 08:00 AM | 6 | 61 | 74 | 27 | 18 | 0 | 30 | 216 |
| 08:15 AM | 20 | 39 | 47 | 21 | 15 | 0 | 30 | 172 |
| 08:30 AM | 21 | 43 | 60 | 23 | 13 | 0 | 33 | 193 |
| 08:45 AM | 14 | 38 | 54 | 25 | 14 | 0 | 33 | 178 |
| Total | 61 | 181 | 235 | 96 | 60 | 0 | 126 | 759 |


| 04:00 PM | 19 | 39 | 61 | 41 | 60 | 0 | 59 | 279 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 04:15 PM | 30 | 51 | 67 | 28 | 71 | 0 | 74 | 321 |
| 04:30 PM | 20 | 45 | 61 | 33 | 68 | 2 | 73 | 302 |
| 04:45 PM | 17 | 52 | 61 | 41 | 81 | 1 | 70 | 323 |
| Total | 86 | 187 | 250 | 143 | 280 | 3 | 276 | 1225 |
| 05:00 PM | 22 | 43 | 63 | 25 | 91 | 1 | 57 | 302 |
| 05:15 PM | 27 | 45 | 58 | 36 | 84 | 0 | 62 | 312 |
| 05:30 PM | 15 | 49 | 83 | 19 | 78 | 1 | 56 | 301 |
| 05:45 PM | 17 | 43 | 70 | 28 | 81 | 1 | 70 | 310 |
| Total | 81 | 180 | 274 | 108 | 334 | 3 | 245 | 1225 |
| Grand Total | 334 | 808 | 1083 | 447 | 729 | 7 | 806 | 4214 |
| Apprch \% | 29.2 | 70.8 | 70.8 | 29.2 | 47.3 | 0.5 | 52.3 |  |
| Total \% | 7.9 | 19.2 | 25.7 | 10.6 | 17.3 | 0.2 | 19.1 |  |


|  | KELLY CREEK PKWY <br> Southbound |  |  | KELLY CREEK PKWY <br> Northbound |  | I-20 EB EXIT RAMP <br> Eastbound |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru App. Total | App. Total | Thru | Right App. Total | Left | Thru | Right | App. Total | Int. Total |

Peak Hour From 07:00 AM to 08:45 AM - Peak 1 of 1

| Intersection | 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume | 106 | 260 | 366 |  |  | 324 | 100 | 424 | 55 | , | 159 | 215 | 1005 |
| Percent | 29.0 | 71.0 |  |  |  | 76.4 | 23.6 |  | 25.6 | 0.5 | 74.0 |  |  |
| 07:15 Volume | 29 | 71 | 100 |  |  | 95 | 20 | 115 | 16 | 1 | 32 | 49 | 264 |
| Peak Factor |  |  |  |  |  |  |  |  |  |  |  |  | 0.952 |
| High Int. | 07:15 AM |  |  | $6: 45: 00$ |  | 07:00 AM |  |  | 07:45 AM |  |  |  |  |
| Volume | 29 | 71 | 100 |  |  | 90 | 29 | 119 | 15 | 0 | 43 | $58$ |  |

Peak Hour From 07:00 AM to 08:45 AM - Peak 1 of 1

| By Approach | $07: 00 \mathrm{AM}$ |  |  |  |
| ---: | :---: | ---: | ---: | ---: |
| Volume | 106 | 260 | 366 |  |
| Percent | 29.0 | 71.0 |  |  |
| High Int. | $07: 15 \mathrm{AM}$ |  | 100 |  |
| Volume | 29 | 71 | 0.915 |  |
| Peak Factor |  |  |  |  |



|  | $07: 00 \mathrm{AM}$ |  |  |  |
| ---: | :---: | ---: | ---: | ---: |
| 424 | 55 | 1 | 159 | 215 |
|  | 25.6 | 0.5 | 74.0 |  |
| 119 | $07: 45$ AM |  |  |  |
| 0.891 |  | 0 | 43 | 58 |
|  |  |  |  | 0.927 |

## TRAFFIC DATA, LLC <br> 1409 Turnham Lane <br> Birmingham, AL 35216 <br> 205-824-0125

File Name : moody03
Site Code : 00000000
Start Date : 01/08/2020
Page No : 2

|  | KELLY CREEK PKWY <br> Southbound |  |  |  | KELLY CREEK PKWY <br> Northbound |  |  | 1-20 EB EXIT RAMPEastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | App. Total | App. Total | Thru | Right | App. Total | Left | Thru | Right | App. Total | Int. Total |
| Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection | 04:15 PM |  |  |  |  |  |  |  |  |  |  |  |
| Volume | 89 | 191 | 280 | 0 | 252 | 127 | 379 | 311 | 4 | 274 | 589 | 1248 |
| Percent | 31.8 | 68.2 |  |  | 66.5 | 33.5 |  | 52.8 | 0.7 | 46.5 |  |  |
| 04:45 Volume | 17 | 52 | 69 | 0 | 61 | 41 | 102 | 81 | 1 | 70 | 152 | 323 |
| Peak Factor |  |  |  |  |  |  |  |  |  |  |  | 0.966 |
| High Int. | 04:15 PM |  |  |  | 04:45 PM |  |  | 04:45 PM |  |  |  |  |
| Volume | 30 | 51 | 81 | 0 | 61 | 41 | 102 | 81 | 1 | 70 | 152 |  |
| Peak Factor |  |  | 0.864 |  |  |  | 0.929 |  |  |  | 0.969 |  |




# TRAFFIC DATA, LLC <br> 1409 Turnham Lane <br> Birmingham, AL 35216 <br> 205-824-0125 

File Name : moody02
Site Code : 00000000
Start Date : 01/08/2020
Page No : 2

|  | KELLY CREEK PKWY <br> Southbound |  |  | 1-20 WB EXIT RAMP Westbound |  |  |  | KELLY CREEK PKWY <br> Northbound |  |  | App. Total | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | Right | App. Total | Left | Thru | Right | App. Total | Left | Thru | App. Total |  |  |
| Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1 Intersection 04:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume | 210 | 156 | 366 | 65 | 1 | 168 | 234 | 116 | 453 | 569 | 0 | 1169 |
| Percent | 57.4 | 42.6 |  | 27.8 | 0.4 | 71.8 |  | 20.4 | 79.6 |  |  |  |
| 05:15 Volume | 59 | 33 | 92 | 17 | 0 | 53 | 70 | 27 | 117 | 144 | 0 | 306 |
| Peak Factor |  |  |  |  |  |  |  |  |  |  |  | 0.955 |
| High Int. | 05:00 PM |  |  | 05:15 PM |  |  |  | 05:00 PM |  |  |  |  |
| Volume | 49 | 48 | 97 | 17 | 0 | 53 | 70 | 37 | 121 | 158 |  |  |
| Peak Factor |  |  | 0.943 |  |  |  | 0.836 |  |  | 0.900 |  |  |

Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1

| By Approach Volume | $04: 15 \mathrm{PM}$ 221 | 151 | 372 | $04: 30 \mathrm{PM}$ 65 | 1 | 168 | 234 | 05:00 PM | 496 | 615 | $\begin{array}{r} 04: 00 \text { PM } \\ 0 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent | 59.4 | 40.6 |  | 27.8 | 0.4 | 71.8 |  | 19.3 | 80.7 |  |  |
| High int. | 04:15 PM |  |  | 05:15 PM |  |  |  | 05:00 PM |  |  | - |
| Volume | 70 | 28 | 98 | 17 | 0 | 53 | 70 | 37 | 121 | 158 |  |
| Peak Factor |  |  | 0.949 |  |  |  | 0.836 |  |  | 0.973 |  |



# TRAFFIC DATA, LLC 

1409 Turnham Lane

Birmingham, AL 35216
205-824-0125

File Name : moody01
Site Code : 00000000
Start Date : 01/08/2020
Page No : 2

|  | KELLY CREEK PKWY <br> Southbound |  |  |  | CR 10 Westbound |  |  |  | KELLY CREEK PKWY <br> Northbound |  |  |  |  | PARK AVE Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | $\begin{array}{r} \text { Righ } \\ t \end{array}$ | App. <br> Total | Left | Thru | $\begin{array}{r} \text { Righ } \\ \mathrm{t} \end{array}$ | App. Total | Left | Thru | $\underset{t}{ }$ | L Int | App. <br> Total | Left | Thru | $\begin{array}{r} \text { Righ } \\ t \end{array}$ | $\begin{array}{r} \mathrm{R} \\ \text { Int } \end{array}$ | App. <br> Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersectio | 05:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume | 4 | 105 | 32 | 141 | 7 | 3 | 1 | 11 | 152 | 442 | 6 | 5 | 605 | 87 | 3 | 156 | 0 | 246 | 1003 |
| Percent | 2.8 | 74.5 | 22.7 |  | 63.6 | 27.3 | 9.1 |  | 25.1 | 73.1 | 1.0 | 0.8 |  | 35.4 | 1.2 | 63.4 | 0.0 |  |  |
| 05:15 | 1 | 29 | 4 | 34 | 1 | 1 | 0 | 2 | 41 | 115 | 2 | 2 | 160 | 28 | 2 | 41 | 0 | 71 | 267 |
| Volume Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.939 |
| Factor |  |  |  |  |  |  |  |  | 05:15 PM |  |  |  |  | 05:15 PM |  |  |  |  |  |
| High Int. | 05:00 PM |  |  |  | 05:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume | 3 | 28 | 11 | 42 | 2 | 2 | 1 | 5 | 41 | 115 | 2 | 2 | 160 | 28 | 2 | 41 | 0 | 71 |  |
| Peak |  |  |  | 0.839 |  |  |  | 0.550 |  |  |  |  | 0.945 |  |  |  |  | 0.866 |  |
| Factor |  |  |  | 0.839 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



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5.4 mph
82.7 mph
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peorls əoed ydum OT

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Total


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39.9 & 32.2
\end{array}
$$

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Level of service criteria for unsignalized intersections is stated in terms of average control delay. Control delay is defined as the total elapsed time from a vehicle joining the queue until its departure from the stopped position at the head of the queue. The criteria for each level of service are cited in the table below.

| Level of <br> Service | Average Control Delay <br> (seconds/vehicle) |
| :---: | :---: |
| A | $0-10$ |
| B | $>10-15$ |
| C | $>15-25$ |
| D | $>25-35$ |
| E | $>35-50$ |
| F | $>50$ |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh 17.4 |  |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ |  | 「 |  |  |  |  | $\uparrow$ | F' |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 55 | 1 | 159 | 0 | 0 | 0 | 0 | 324 | 100 | 106 | 260 | 0 |
| Future Vol, veh/h | 55 | 1 | 159 | 0 | 0 | 0 | 0 | 324 | 100 | 106 | 260 | 0 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.89 | 0.89 | 0.89 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 21 | 21 | 21 | 2 | 2 | 2 | 2 | 21 | 21 | 10 | 10 | 2 |
| Mvmt Flow | 59 | 1 | 171 | 0 | 0 | 0 | 0 | 364 | 112 | 115 | 283 | 0 |
| Number of Lanes | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  |  |  |  |  | NB |  | SB |  |  |
| Opposing Approach |  |  |  |  |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 0 |  |  |  |  |  |  | 1 |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  |  |  |  |  | EB |  |  |  |  |
| Conflicting Lanes Left | 1 |  |  |  |  |  |  | 2 |  | 0 |  |  |
| Conflicting Approach Right | NB |  |  |  |  |  |  |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  |  |  |  |  | 0 |  | 2 |  |  |
| HCM Control Delay | 12 |  |  |  |  |  |  | 16.6 |  | 21.5 |  |  |
| HCM LOS | B |  |  |  |  |  |  | C |  | C |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $29 \%$ |
| Vol Thu, \% | $100 \%$ | $0 \%$ | $0 \%$ | $1 \%$ | $71 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $99 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 324 | 100 | 55 | 160 | 366 |
| LT Vol | 0 | 0 | 55 | 0 | 106 |
| Through Vol | 324 | 0 | 0 | 1 | 260 |
| RT Vol | 0 | 100 | 0 | 159 | 0 |
| Lane Flow Rate | 364 | 112 | 59 | 172 | 398 |
| Geometry Grp | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.626 | 0.171 | 0.127 | 0.311 | 0.683 |
| Departure Headway (Hd) | 6.194 | 5.484 | 7.727 | 6.508 | 6.178 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 582 | 654 | 464 | 552 | 585 |
| Service Time | 3.931 | 3.221 | 5.477 | 4.258 | 4.214 |
| HCM Lane V/C Ratio | 0.625 | 0.171 | 0.127 | 0.312 | 0.68 |
| HCM Control Delay | 18.8 | 9.4 | 11.6 | 12.2 | 21.5 |
| HCM Lane LOS | C | A | B | B | C |
| HCM 95th-tile Q | 4.3 | 0.6 | 0.4 | 1.3 | 5.3 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 8.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | SEL | SET | SER | NWL | NWT | NWR |  |
| Lane Configurations |  | * |  |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |  | * |  |  |
| Traffic Vol, veh/h | 126 | 108 | 7 | 6 | 616 | 88 | 30 | 6 | 145 | 14 | 2 | 1 |  |
| Future Vol, veh/h | 126 | 108 | 7 | 6 | 616 | 88 | 30 | 6 | 145 | 14 | 2 | 1 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | Yield | - | - | Yield | - | - | None |  |
| Storage Length | - | - | - | - | - | 95 | - | - | 150 | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 84 | 84 | 84 | 91 | 91 | 91 | 60 | 60 | 60 | 47 | 47 | 47 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 150 | 129 | 8 | 7 | 677 | 97 | 50 | 10 | 242 | 30 | 4 | 2 |  |





| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 18.9$ |  |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ |  | 「 |  |  |  |  | 4 | 「 |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 324 | 4 | 262 | 0 | 0 | 0 | 0 | 243 | 135 | 86 | 185 | 0 |
| Future Vol, veh/h | 324 | 4 | 262 | 0 | 0 | 0 | 0 | 243 | 135 | 86 | 185 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.92 | 0.92 | 0.92 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles, \% | 21 | 21 | 21 | 2 | 2 | 2 | 2 | 21 | 21 | 10 | 10 | 2 |
| Mvmt Flow | 334 | 4 | 270 | 0 | 0 | 0 | 0 | 261 | 145 | 91 | 197 | 0 |
| Number of Lanes | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  |  |  |  |  | NB |  | SB |  |  |
| Opposing Approach |  |  |  |  |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 0 |  |  |  |  |  |  | 1 |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  |  |  |  |  | EB |  |  |  |  |
| Conflicting Lanes Left | 1 |  |  |  |  |  |  | 2 |  | 0 |  |  |
| Conflicting Approach Right | NB |  |  |  |  |  |  |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  |  |  |  |  | 0 |  | 2 |  |  |
| HCM Control Delay | 20.9 |  |  |  |  |  |  | 15.7 |  | 19.3 |  |  |
| HCM LOS | C |  |  |  |  |  |  | C |  | C |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $32 \%$ |
| Vol Thru, \% | $100 \%$ | $0 \%$ | $0 \%$ | $2 \%$ | $68 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $98 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 243 | 135 | 324 | 266 | 271 |
| LT Vol | 0 | 0 | 324 | 0 | 86 |
| Through Vol | 243 | 0 | 0 | 4 | 185 |
| RT Vol | 0 | 135 | 0 | 262 | 0 |
| Lane Flow Rate | 261 | 145 | 334 | 274 | 288 |
| Geometry Grp | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.527 | 0.264 | 0.697 | 0.48 | 0.571 |
| Departure Headway (Hd) | 7.266 | 6.551 | 7.508 | 6.299 | 7.132 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 494 | 546 | 481 | 570 | 505 |
| Service Time | 5.038 | 4.322 | 5.268 | 4.058 | 5.196 |
| HCM Lane V/C Ratio | 0.528 | 0.266 | 0.694 | 0.481 | 0.57 |
| HCM Control Delay | 17.9 | 11.7 | 25.9 | 14.8 | 19.3 |
| HCM Lane LOS | C | B | D | B | C |
| HCM 95th-tile Q | 3 | 1.1 | 5.3 | 2.6 | 3.5 |




| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  | ${ }^{7}$ |  | 「゙ |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 65 | 1 | 168 | 116 | 453 | 0 | 0 | 210 | 156 |
| Future Vol, veh/h | 0 | 0 | 0 | 65 | 1 | 168 | 116 | 453 | 0 | 0 | 210 | 156 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | Yield |
| Storage Length | - | - | - | 0 | - | 0 | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 2 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | -3 | - |
| Peak Hour Factor | 92 | 92 | 92 | 84 | 84 | 84 | 90 | 90 | 90 | 94 | 94 | 94 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 13 | 2 | 13 | 12 | 12 | 2 | 2 | 5 | 5 |
| Mvmt Flow | 0 | 0 | 0 | 77 | 1 | 200 | 129 | 503 | 0 | 0 | 223 | 166 |



APPENDIX E
Future Conditions Capacity Analysis

| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh 19.5 |  |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ |  | 「 |  |  |  |  | 4 | 「 |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 93 | 1 | 159 | 0 | 0 | 0 | 0 | 337 | 100 | 113 | 267 | 0 |
| Future Vol, veh/h | 93 | 1 | 159 | 0 | 0 | 0 | 0 | 337 | 100 | 113 | 267 | 0 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.92 | 0.92 | 0.92 | 0.89 | 0.89 | 0.89 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles, \% | 21 | 21 | 21 | 2 | 2 | 2 | 2 | 21 | 21 | 10 | 10 | 2 |
| Mumt Flow | 100 | 1 | 171 | 0 | 0 | 0 | 0 | 379 | 112 | 123 | 290 | 0 |
| Number of Lanes | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  |  |  |  |  | NB |  | SB |  |  |
| Opposing Approach |  |  |  |  |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 0 |  |  |  |  |  |  | 1 |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  |  |  |  |  | EB |  |  |  |  |
| Conflicting Lanes Left | 1 |  |  |  |  |  |  | 2 |  | 0 |  |  |
| Conflicting Approach Right | NB |  |  |  |  |  |  |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  |  |  |  |  | 0 |  | 2 |  |  |
| HCM Control Delay | 12.6 |  |  |  |  |  |  | 18.7 |  | 24.9 |  |  |
| HCM LOS | B |  |  |  |  |  |  | C |  | C |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $30 \%$ |
| Vol Thru, \% | $100 \%$ | $0 \%$ | $0 \%$ | $1 \%$ | $70 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $99 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 337 | 100 | 93 | 160 | 380 |
| LT Vol | 0 | 0 | 93 | 0 | 113 |
| Through Vol | 337 | 0 | 0 | 1 | 267 |
| RT Vol | 0 | 100 | 0 | 159 | 0 |
| Lane Flow Rate | 379 | 112 | 100 | 172 | 413 |
| Geometry Grp | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.673 | 0.178 | 0.218 | 0.317 | 0.731 |
| Departure Headway (Hd) | 6.402 | 5.69 | 7.852 | 6.632 | 6.367 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 564 | 629 | 456 | 540 | 566 |
| Service Time | 4.151 | 3.439 | 5.613 | 4.392 | 4.414 |
| HCM Lane V/C Ratio | 0.672 | 0.178 | 0.219 | 0.319 | 0.73 |
| HCM Control Delay | 21.4 | 9.7 | 12.8 | 12.5 | 24.9 |
| HCM Lane LOS | C | A | B | B | C |
| HCM 95th-tile Q | 5.1 | 0.6 | 0.8 | 1.4 | 6.1 |




| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 14.6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | SEL | SET | SER | NWL | NWT | NWR |
| Lane Configurations |  | $\ddagger$ |  |  | $\uparrow$ | 「 |  | $\uparrow$ | F |  | $\ddagger$ |  |
| Traffic Vol, veh/h | 126 | 172 | 7 | 6 | 652 | 103 | 57 | 6 | 145 | 14 | 2 | 1 |
| Future Vol, veh/h | 126 | 172 | 7 | 6 | 652 | 103 | 57 | 6 | 145 | 14 | 2 | 1 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | Yield | - | - | Yield | - | - | None |
| Storage Length | - | - | - | - | - | 95 | - | - | 150 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 84 | 84 | 84 | 91 | 91 | 91 | 60 | 60 | 60 | 47 | 47 | 47 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 150 | 205 | 8 | 7 | 716 | 113 | 95 | 10 | 242 | 30 | 4 | 2 |





| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 22.5$ |  |
| Intersection LOS | C |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ |  | 「 |  |  |  |  | 4 | 「 |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 356 | 4 | 262 | 0 | 0 | 0 | 0 | 254 | 135 | 104 | 203 | 0 |
| Future Vol, veh/h | 356 | 4 | 262 | 0 | 0 | 0 | 0 | 254 | 135 | 104 | 203 | 0 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.92 | 0.92 | 0.92 | 0.93 | 0.93 | 0.93 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles, \% | 21 | 21 | 21 | 2 | 2 | 2 | 2 | 21 | 21 | 10 | 10 | 2 |
| Mvmt Flow | 367 | 4 | 270 | 0 | 0 | 0 | 0 | 273 | 145 | 111 | 216 | 0 |
| Number of Lanes | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 0 |
| Approach | EB |  |  |  |  |  |  | NB |  | SB |  |  |
| Opposing Approach |  |  |  |  |  |  |  | SB |  | NB |  |  |
| Opposing Lanes | 0 |  |  |  |  |  |  | 1 |  | 2 |  |  |
| Conflicting Approach Left | SB |  |  |  |  |  |  | EB |  |  |  |  |
| Conflicting Lanes Left | 1 |  |  |  |  |  |  | 2 |  | 0 |  |  |
| Conflicting Approach Right | NB |  |  |  |  |  |  |  |  | EB |  |  |
| Conflicting Lanes Right | 2 |  |  |  |  |  |  | 0 |  | 2 |  |  |
| HCM Control Delay | 25.6 |  |  |  |  |  |  | 17.1 |  | 23.5 |  |  |
| HCM LOS | D |  |  |  |  |  |  | C |  | C |  |  |


| Lane | NBLn1 | NBLn2 | EBLn1 | EBLn2 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $34 \%$ |
| Vol Thru, \% | $100 \%$ | $0 \%$ | $0 \%$ | $2 \%$ | $66 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $98 \%$ | $0 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 254 | 135 | 356 | 266 | 307 |
| LT Vol | 0 | 0 | 356 | 0 | 104 |
| Through Vol | 254 | 0 | 0 | 4 | 203 |
| RT Vol | 0 | 135 | 0 | 262 | 0 |
| Lane Flow Rate | 273 | 145 | 367 | 274 | 327 |
| Geometry Grp | 7 | 7 | 7 | 7 | 6 |
| Degree of Util (X) | 0.568 | 0.273 | 0.783 | 0.493 | 0.66 |
| Departure Headway (Hd) | 7.481 | 6.764 | 7.685 | 6.474 | 7.28 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes |
| Cap | 481 | 528 | 470 | 554 | 493 |
| Service Time | 5.264 | 4.546 | 5.457 | 4.244 | 5.351 |
| HCM Lane V/C Ratio | 0.568 | 0.275 | 0.781 | 0.495 | 0.663 |
| HCM Control Delay | 19.7 | 12.1 | 33.2 | 15.4 | 23.5 |
| HCM Lane LOS | C | B | D | C | C |
| HCM 95th-tile Q | 3.5 | 1.1 | 7 | 2.7 | 4.7 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |







APPENDIX F
Turn Lane Warrant Evaluations

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

## INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, mph: | 45 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $44 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 207 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 671 |

## OUTPUT

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 157 |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

## 2-lane roadway (English)

## INPUT

| Variable | Value |
| :--- | :---: |
| $85^{\text {th }}$ percentile speed, $\mathrm{mph}:$ | 45 |
| Percent of left-turns in advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right), \%:$ | $16 \%$ |
| Advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 497 |
| Opposing volume $\left(\mathrm{V}_{\mathrm{O}}\right)$, veh $/ \mathrm{h}:$ | 138 |

## OUTPUT

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting advancing volume $\left(\mathrm{V}_{\mathrm{A}}\right)$, veh/h: | 376 |
| Guidance for determining the need for a major-road left-turn bay: |  |
| Left-turn treatment warranted. |  |



CALIBRATION CONSTANTS

| Variable | Value |
| :--- | :---: |
| Average time for making left-turn, s: | 3.0 |
| Critical headway, s: | 5.0 |
| Average time for left-turn vehicle to clear the advancing lane, s: | 1.9 |

Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadw ay |  |
| :--- | :---: | :---: |
| Variable |  | Value |
| Major-road speed, mph: | 45 |  |
| Major-road volume (one direction), veh/h: | 671 |  |
| Right-turn volume, veh/h: | 37 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 25 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Add right-turn bay. |  |



Figure 2-6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.
INPUT

| Roadway geometry: | 2-lane roadw ay |  |
| :--- | :---: | :---: |
| Variable |  | Value |
| Major-road speed, mph: | 45 |  |
| Major-road volume (one direction), veh/h: | 138 |  |
| Right-turn volume, veh/h: | 31 |  |

OUTPUT

| Variable | Value |
| :--- | :---: |
| Limiting right-turn volume, veh/h: | 457 |
| Guidance for determining the need for a major-road <br> right-turn bay for a 2-lane roadway: |  |
| Do NOT add right-turn bay. |  |



